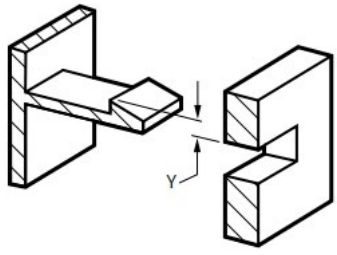


Snap Fit Design

Best practices For Additive Manufacturing Processes

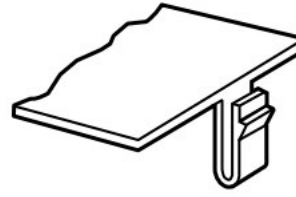
Common Examples



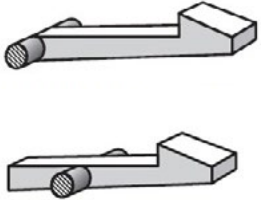
Cantilever



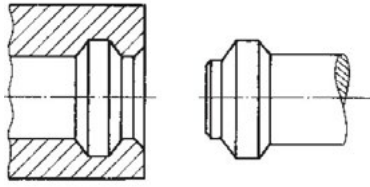
L-Shaped Cantilever



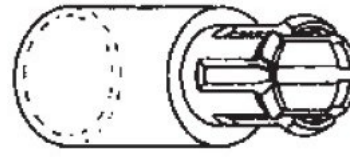
U-Shaped Cantilever



Torsion (Inseparable, and Separable)



Annular



Discontinuous annular snap joint
Also called: Segmented Cantilever in circular format

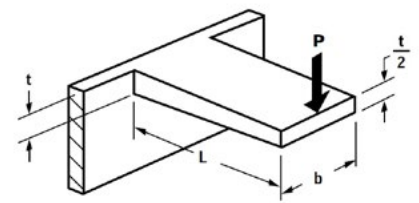
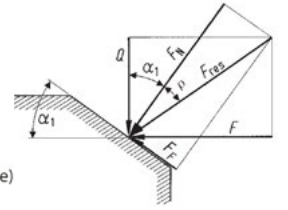
Snap-fit parts allow assembly without tools for thermoplastic components that fit together. They can be permanent or removable, depending on the design and material pairing criteria.

Additive Manufacturing (AM) affords opportunities for useful application of snap-fit geometry in prototyping attachment modes often associated with injection molding processes. While there are few tooling costs associated with part production through AM processes, it is still necessary to consider build orientation and material selection when designing snap-fits to optimize part integrity and function.

Important considerations when implementing a snap-fit joint are material resilience and elasticity, permitted strain, deflection, clearances and build orientation to prevent staircase effects.

Applied Forces

Q = Deflection force
 F = Assembly force
 F_N = Normal force
 F_f = Friction force
 F_{res} = Resultant force
 α_1 = Joining angle (lead-in angle)
 ρ = Friction angle



II) Uniform Width, Height Tapers to $t/2$ at Free End

$$\text{Stiffness: } k = \frac{P}{Y} = \frac{Eb}{6.528} \left(\frac{t}{L}\right)^3$$

$$\text{Strain: } \epsilon = 0.92 \left(\frac{t}{L^2}\right) Y$$

Where:
 E = Flexural Modulus
 P = Force
 Y = Deflection
 b = Width of Beam

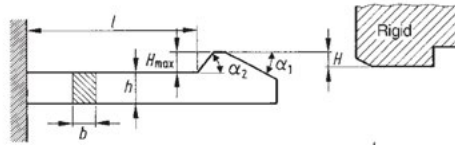
For more on strain calculation, check out the BASF Snap-Fit DesignGuide in the resources section

Cantilever Snap-Fit

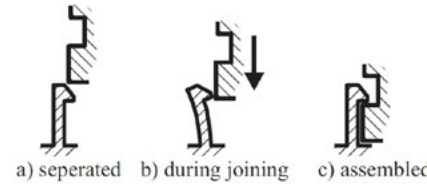
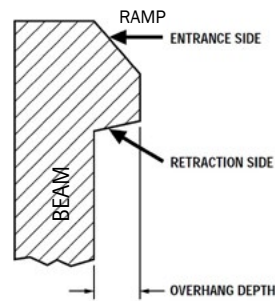
- Successful design must find a balance between integrity of the assembly (stays latched) and strength of the cantilever beam (doesn't degrade with repeated stress).
- The depth of the overhang defines the amount of deflection during assembly.
- A cantilever beam with a deep overhang can make the unit secure, but it also puts more strain on the beam during assembly and disassembly.
- The overhang typically has a gentle ramp on the entrance side and a sharper angle on the retraction side.
- A small angle at the entrance side helps to reduce the assembly effort.
- A sharp angle at the retraction side (hook) makes disassembly very difficult or impossible depending on the intended function.
- Locators help the user to align the parts and guide the movement until a snapping sound indicates that the connection is made.
- Tapering the beam helps reduce strain on the material and allows more deflection without permanent deformation of the beam material.
- Choose the direction of deflection independently of the given joining direction if it works better with build orientation.
- Consider the amount of deflection carefully - Large deflection amounts may cause delamination in FDM beam structures.
- Stress concentrations are typically found in sharp corners, try to fillet joints to reduce strain.

Angles and Clearance Dimensions

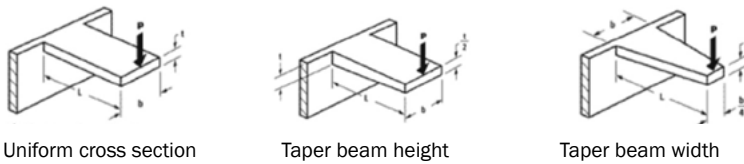
α_1 = Joining angle
 α_2 = Retaining angle
 b = Breadth of cross section (hook breadth)
 h = Height of cross section
 l = Snap-fit length
 H = Snap-fit height (undercut)



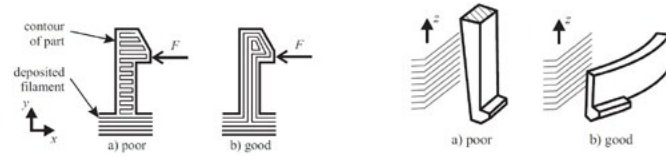
Deflection



Increase flexibility by removing material

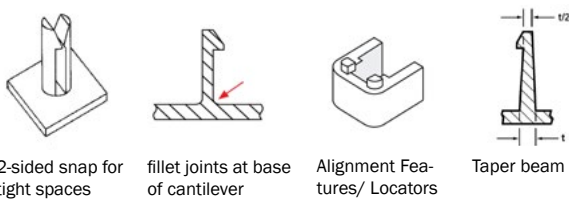


FDM Print Build Alignment



During snap-fit joining the material is stressed along the stronger directions of the anisotropic material and the notches between layers have less impact on the durability of the cantilever beam. Consider extrusion head tool path in configuring design elements and build orientation to yield highest level of part integrity.

Design to Reduce Material Loading



Annular Snap Fit

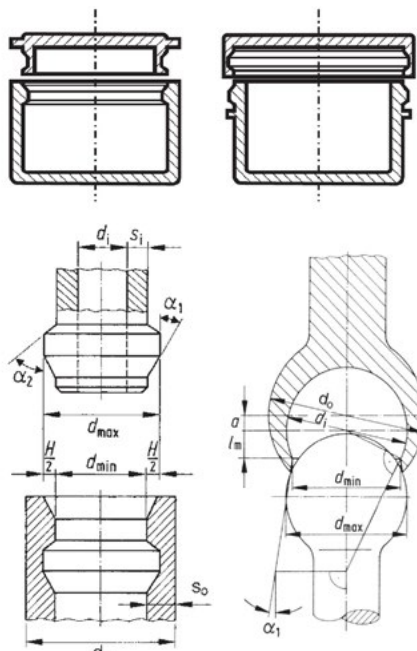
Annular or circular snap-fits are rotationally symmetrical and involve multiaxial stresses. Annular snap-fits rely on the elastic properties of thermoplastic to expand and compress to allow limited clearances to expand to assemble parts. Thermoplastic material selection criteria must include elastic properties to allow circumference to compress or elongate.

Clearance - difference between greatest diameter and smallest diameter. If producing on FDM equipment design clearance of .012" (.35mm)

Wall thickness on the outer deflecting (flexing) part. For FDM production not thicker than .075" (1.9 mm)

Dimensions and their designations in cylindrical annular snap-fit joints

d_{max} = Greatest diameter } of the snap-fit joint
 d_{min} = Smallest diameter }
 d_o = Outer diameter } of the outer part
 s_o = Wall thickness }
 d_i = Inner diameter } of the inner part
 s_i = Wall thickness }



Torsion Snap Fit

Torsion snap-fits rely on rotation about an axis that is fixed in location. Some torsion designs use a removable design like a see-saw - A push on the free end of the beam lifts the hook and releases the joint.

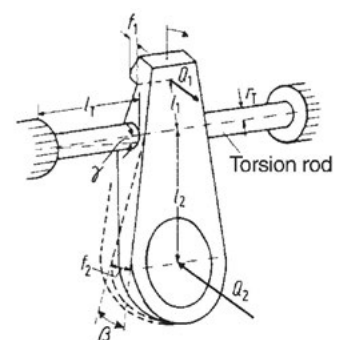
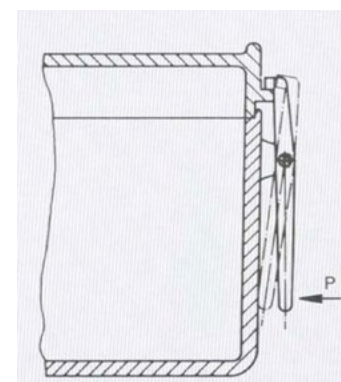


Figure 8.7 Dimensions and their designations in torsional snap-fit joints

l_T = Length } of torsion rod
 r_T = Radius }
 β = Torsion angle
 γ = Twisting angle
 $l_{1,2}$ = Lever arm lengths
 $f_{1,2}$ = Elastic excursions
 $Q_{1,2}$ = Deflection forces



References

1. Designing with Plastics, Gunter Erhard
 Leseprobe 2, Weitere Informationen oder Bestellungen unter
<http://www.hanser.de/3-446-22590-0>
 ISBN 3-446-22590-0

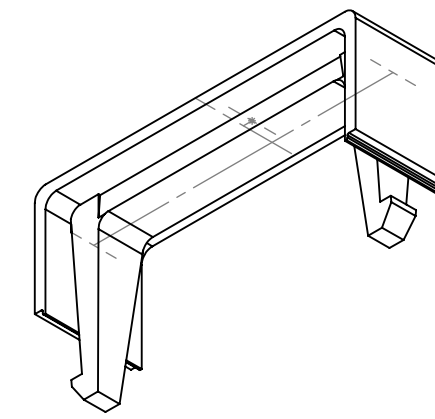
2. Design Guidelines for Additive Manufactured Snap-Fit Joints
 Christoph Klahn*, Daniel Singer, Mirko Meboldt
 Inspire AG, Leonhardstrasse 21, 8092 Zurich, Switzerland

3. BASF Snapfit guidelines, 2007

4. Troughton, Michael J., and Institute of Welding International. Handbook of Plastics Joining : A Practical Guide, Elsevier Science & Technology Books, 2008. ProQuest Ebook Central, <https://ebookcentral-proquest-com.proxy1.lib.tju.edu/lib/philau/detail.action?docID=428695>.

5. Bayer Material Science LLC, Snap-fit joints for plastics - a design guide, Pittsburg (2013).

Scoring:
 Engagement - how difficult is it to seat the snap correctly
 Disengagement - how difficult is it to disassemble the snap
 Integrity - how well does it hold



All test snap hooks shared same height and the same receiving slot for continuity
 Snap Hook Beam length overall .866" (22 mm)

Beam
 Thickness
 Initial: .118" (3.0mm)
 Terminal: .079" (2.0mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 3 deg
 Overhang: .079" (2.0mm)
 Ramp: .118" (3.0mm)
 Snap hook height: .039" (1.0mm)

score
Engagement: 3
Disengagement: 4
Integrity: 4

Beam
 Thickness
 Initial: .118" (3.0mm)
 Terminal: .059" (1.5mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 4 deg
 Overhang: .079" (2.0mm)
 Ramp: .118" (3.0mm)
 Snap hook height: .0" (0mm)

score
Engagement: 3
Disengagement: 4
Integrity: 3

Beam
 Thickness
 Initial: .118" (3.0mm)
 Terminal: .079" (2.0mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 3 deg
 Overhang: .079" (2.0mm)
 Ramp: .157" (4.0mm)
 Snap hook height: .039" (1.0mm)

score
Engagement: 3
Disengagement: 3
Integrity: 4

Beam
 Thickness
 Initial: .197" (5.0mm)
 Terminal: .071" (1.8mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 5 deg
 Overhang: .079" (2.0mm)
 Ramp: .157" (4.0mm)
 Snap hook height: .02" (.5mm)

score
Engagement: 3
Disengagement: 2
Integrity: 5

Beam
 Thickness
 Initial: .118" (3.0mm)
 Terminal: .079" (2.0mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 3 deg
 Ramp: .118" (3.0mm)
 Snap hook height: .039" (1.0mm)

score
Engagement: 4
Disengagement: 4
Integrity: 4

Beam
 Thickness
 Initial: .197" (5.0mm)
 Terminal: .118" (3.0mm)
 Width
 Initial: .157" (4.0mm)
 Taper: 5 deg
 Overhang: .079" (2.0mm)
 Ramp: .157" (4.0mm)
 Snap hook height: .039" (1.0mm)

score
Engagement: 3
Disengagement: 1
Integrity: 5

Type of design		Shape of the cross section			
		A Rectangle	B Trapezoid	C Ring segment	D Irregular cross section
(Permissible) deflection	1 Cross section constant Over the length	$y = 0.67 \cdot \frac{\epsilon \cdot l^2}{h}$	$y = \frac{a + b_{(1)}}{2a + b} \cdot \frac{\epsilon \cdot l^2}{h}$	$y = K_{(2)} \cdot \frac{\epsilon \cdot l^2}{r_2}$	$y = \frac{1}{3} \cdot \frac{\epsilon \cdot l^2}{c_{(2)}}$
	2 All dimensions in direction y, e.g., h or Δr, decrease to One-half	$y = 1.09 \cdot \frac{\epsilon \cdot l^2}{h}$	$y = 1.64 \cdot \frac{a + b_{(1)}}{2a + b} \cdot \frac{\epsilon \cdot l^2}{h}$	$y = 1.64 \cdot K_{(2)} \cdot \frac{\epsilon \cdot l^2}{r_2}$	$y = 0.55 \cdot \frac{\epsilon \cdot l^2}{c_{(2)}}$
	3 All dimensions in direction z, e.g., b and a, decrease to one-quarter	$y = 0.86 \cdot \frac{\epsilon \cdot l^2}{h}$	$y = 1.28 \cdot \frac{a + b_{(1)}}{2a + b} \cdot \frac{\epsilon \cdot l^2}{h}$	$y = 1.28 \cdot K_{(2)} \cdot \frac{\epsilon \cdot l^2}{r_2}$	$y = 0.43 \cdot \frac{\epsilon \cdot l^2}{c_{(2)}}$
Deflection force	1,2,3	$P = \frac{bh^2}{6} \cdot \frac{E_s \epsilon}{l}$	$P = \frac{h^2}{12} \cdot \frac{a^2 + 4ab_{(1)} + b^2}{2a + b} \cdot \frac{E_s \epsilon}{l}$	$P = Z_{(4)} \cdot \frac{E_s \epsilon}{l}$	$P = Z_{(4)} \cdot \frac{E_s \epsilon}{l}$

Subscript numbers in parenthesis designate the note to refer to.

Symbols

- y = (permissible) deflection (=undercut)
- E = (permissible) strain in the outer fiber
- at the root; in formulae: E as absolute value = percentage/100 (see Table 2)
- l = length of arm
- h = thickness at root
- b = width at root
- c = distance between outer fiber and neutral fiber (center of gravity)
- Z = section modulus $Z = I c$, where I = axial moment of inertia
- E_s = secant modulus (see Fig. 16)
- P = (permissible) deflection force
- K = geometric factor (see Fig. 10)